

# Pre-mission error assessment for the pendulum formation via the semi-analytical approach

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**GIS**

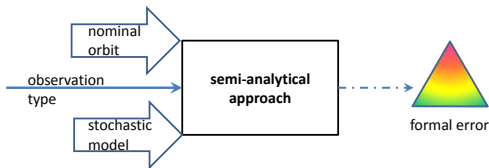


Fig: scheme of the semi-analytical approach

- + very effective error assessment
- + no observation data
- constant orbital parameters
- constant gravity field
- representation in lumped coefficients required

# Semi-analytical approach

- 1 rotating Hill-frame
- 2 lumped coefficient = 2D Fourier series

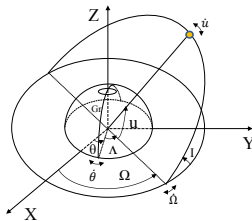
$$f^{\#} = \sum_{m=-\infty}^{\infty} \sum_{k=-\infty}^{\infty} A_{mk}^{\#} e^{i(ku+m\Lambda)}$$

$$A_{mk}^{\#} = \sum_{l=\max(|m|,|k|)}^{\infty} H_{lmk}^{\#} \bar{K}_{lm}$$

$f^{\#}$ : specific observable

$H_{lmk}^{\#}$ : transfer coefficients

$\bar{K}_{lm}$ : gravity field coefficients



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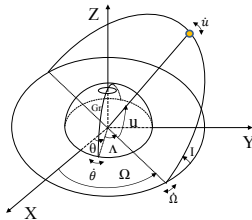
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circular case:  $\psi_{kmt} = (ku + m\Lambda)$



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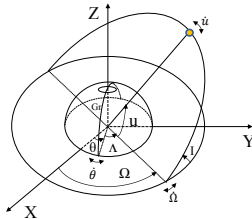
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- 3 error propagation in matrix form:

$$\underline{\mathbf{Q}}_{xx} = \left[ \left( \underline{\mathbf{H}}_{lmk}^\# \right)^\top \underline{\mathbf{P}} \left( \underline{\mathbf{H}}_{lmk}^\# \right) \right]^{-1} \Rightarrow \delta \bar{\mathbf{K}}_{lm} \Rightarrow \{ \delta \bar{\mathbf{C}}_{lm}, \delta \bar{\mathbf{S}}_{lm} \}$$

# Hill differential equation

orbit perturbations in rotating frame:

$$\ddot{x} + 2n\dot{z} = \sum_{l,m,k} \frac{GM}{R^2} \left(\frac{R}{r}\right)^{l+2} {}_l k \bar{F}_{lmk}(l) \bar{K}_{lm} e^{i\psi_{km}t}$$

$$\ddot{y} + n^2 y = \sum_{l,m,k} \frac{GM}{R^2} \left(\frac{R}{r}\right)^{l+2} \bar{F}_{lmk}^*(l) \bar{K}_{lm} e^{i\psi_{km}t}$$

$$\ddot{z} - 2n\dot{x} - 3n^2 z = \sum_{l,m,k} \frac{GM}{R^2} \left(\frac{R}{r}\right)^{l+2} (-l-1) k \bar{F}_{lmk}(l) \bar{K}_{lm} e^{i\psi_{km}t}$$

- $n$ : natural orbit frequency ( $n^2 r^3 = GM$ )
- disturbing force = gravity gradient in rotation frame
- (cross-track) **inclination function**  $\bar{F}_{lmk}(l)$  ( $\bar{F}_{lmk}^*(l)$ )

# Transfer coefficients of orbit perturbations

Transfer coefficients of particular solution:

$$H_{lmk}^{\Delta x} = \frac{2(l+1)\dot{\psi}_{mk}n - k(\dot{\psi}_{mk}^2 + 3n^2)}{\dot{\psi}_{mk}^2(\dot{\psi}_{mk}^2 - n^2)} \frac{GM}{R^2} \left(\frac{R}{r}\right)^{l+2} \bar{F}_{lmk}(l)$$

$$H_{lmk}^{\Delta y} = \frac{1}{n^2 - \dot{\psi}_{mk}^2} \frac{GM}{R^2} \left(\frac{R}{r}\right)^{l+2} \bar{F}_{lmk}^*(l)$$

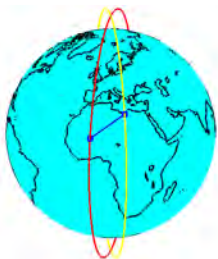
$$H_{lmk}^{\Delta z} = \frac{(l+1)\dot{\psi}_{mk} - 2kn}{\dot{\psi}_{mk}^2(\dot{\psi}_{mk}^2 - n^2)} \frac{GM}{R^2} \left(\frac{R}{r}\right)^{l+2} \bar{F}_{lmk}(l)$$

orbit perturbations

$$\Delta x(t) = \sum_{l,m,k} H_{lmk}^{\Delta x} \bar{K}_{lm} e^{i\psi_{kmt}}$$

...

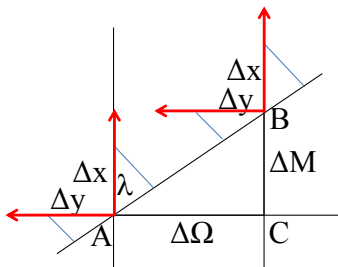
# Pendulum constellation



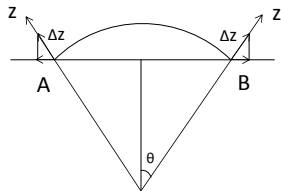
- 2 satellites on circular orbits
  - same inclination  $i$  and radius  $r$
  - different ascending node  $\Delta\Omega$
  - 'time lag'  $\Delta M$  between satellites
- 
- observation: range, range rate, range acceleration
  - time dependent opening angle  
( $\Rightarrow$  along-track and cross-track observations)



# Range rate perturbation



(a) along/cross track directions  
A: reference satellite



(b) radial direction

planar approximation

$$\Delta\rho(t) = (\Delta x_B - \Delta x_A) \cos \lambda + (\Delta y_A - \Delta y_B) \sin \lambda + (\Delta z_B + \Delta z_A) \sin \theta$$

## Orbit perturbations

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$$\Delta\rho(t) = (\Delta x_B - \Delta x_A) \cos \lambda + (\Delta y_A - \Delta y_B) \sin \lambda \\ + (\Delta z_B + \Delta z_A) \sin \theta$$

# Orbit perturbations

$$\Delta\rho(t) = (\Delta x_B - \Delta x_A) \cos \lambda + (\Delta y_A - \Delta y_B) \sin \lambda \\ + (\Delta z_B + \Delta z_A) \sin \theta$$

components:

$$\Delta x_B - \Delta x_A = \sum_{l,m,k} H_{lmk}^{\Delta x} \left( e^{i(\beta_{mk} \Delta M + m \Delta \Omega)} - 1 \right) \bar{K}_{lm} e^{i\psi_{km} t}$$

$$\Delta y_A - \Delta y_B = \sum_{l,m,k} H_{lmk}^{\Delta y} \left( 1 - e^{i(\beta_{mk} \Delta M + m \Delta \Omega)} \right) \bar{K}_{lm} e^{i\psi_{km} t}$$

$$\Delta z_A + \Delta z_B = \sum_{l,m,k} H_{lmk}^{\Delta z} \left( e^{i(\beta_{mk} \Delta M + m \Delta \Omega)} + 1 \right) \bar{K}_{lm} e^{i\psi_{km} t}$$

with  $\beta_{mk} = k + m \frac{\dot{\Lambda}}{U}$

# Time-variable orbital elements

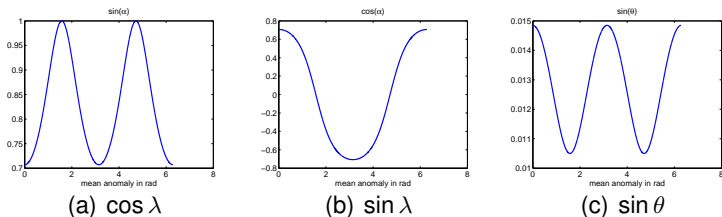


Fig: time variable components for  $\rho_x = \rho_{y,max} = 141$  km ( $\lambda = 45^\circ$ )

$$\cos \lambda = \sum_{k'=-K}^K A_{k'} e^{ik' \dot{u} t}, \quad \sin \lambda = \sum_{k'=-K}^K B_{k'} e^{ik' \dot{u} t},$$
$$\sin \theta = \sum_{k'=-K}^K C_{k'} e^{ik' \dot{u} t}$$

- numerical FFT
- recursion formula (elliptic integrals)

# Transfer coefficients of the pendulum formation

$$H_{Imp}^{\Delta\rho(t)} = H_{Imp}^{\Delta\rho(t)x} + H_{Imp}^{\Delta\rho(t)y} + H_{Imp}^{\Delta\rho(t)z} \quad \text{with}$$

$$H_{Imp}^{\Delta\rho(t)x} = \sum_{k'=-K}^K A_{k'} H_{Im(p-k')}^{\Delta x} \left( e^{\imath(\beta_{m(p-k')}\Delta M + m\Delta\Omega)} - 1 \right)$$

$$H_{Imp}^{\Delta\rho(t)y} = \sum_{k'=-K}^K B_{k'} H_{Im(p-k')}^{\Delta x} \left( 1 - e^{\imath(\beta_{m(p-k')}\Delta M + m\Delta\Omega)} \right)$$

$$H_{Imp}^{\Delta\rho(t)z} = \sum_{k'=-K}^K C_{k'} H_{Im(p-k')}^{\Delta x} \left( e^{\imath(\beta_{m(p-k')}\Delta M + m\Delta\Omega)} + 1 \right)$$

new index  $p = k + k'$

# Effect of Fourier series

terms like  $\sum_{k'=-K}^K A_{k'} H_{lm}^{\Delta x(p-k')}$  describe a convolution

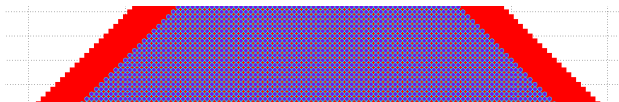


Fig: non-zero elements of transfer matrix for degree  $l = 60$ ,  $m = 20$ ,  
 $K = 9$  (blue: GRACE, red+blue: pendulum)

# Formal error for range rate

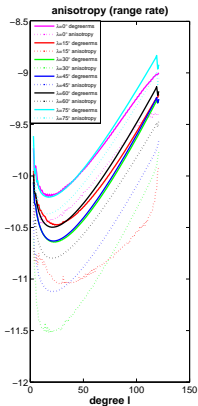
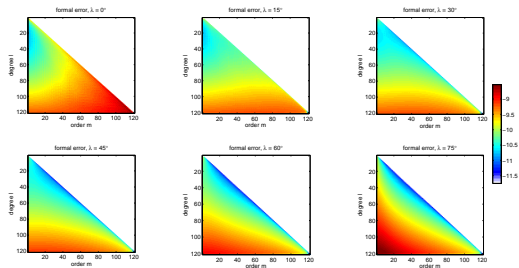


Fig:  $\beta/\alpha = 490/31$ ,  $\rho_{max} = 200$  km,  $h = 308$  km  
and  $psd = 5 \cdot 10^{-5} \text{ m/s}^2/\sqrt{\text{Hz}}$

- most homogeneous error pattern for  $\lambda \approx 30^\circ$
- smallest formal errors  $30^\circ - 45^\circ$

# Formal error for range acceleration

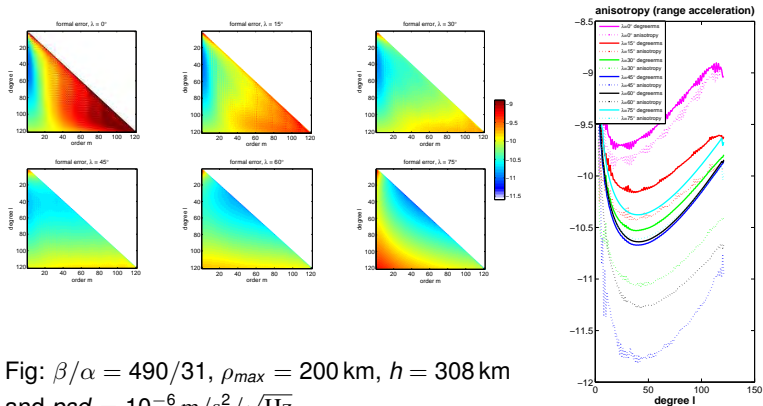


Fig:  $\beta/\alpha = 490/31$ ,  $\rho_{max} = 200$  km,  $h = 308$  km  
and  $psd = 10^{-6} \text{ m/s}^2/\sqrt{\text{Hz}}$

- most homogeneous error pattern for  $\lambda \approx 45^\circ$
- smallest formal errors  $45^\circ - 60^\circ$



# Summary

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- (optimistic) error assessment by semi-analytical approach
- orbit perturbations via Hill differential equation
- special problem: time-dependent opening angle
  - Fourier series (with closed formulas)
  - convolution
- optimal angle depends on observation type
- spectral pattern of minimal formal error for
  - low degree
  - near sectorials